

# Column effective length

Effective length and slenderness of a column · EN 1992-1-1 §5.8.3 · UK NA / PN-EN

|                |                                                                                                           |
|----------------|-----------------------------------------------------------------------------------------------------------|
| Reference      | NAE-RC-037 · version 1.0                                                                                  |
| Standards      | BS EN 1992-1-1:2004 with UK NA · PN-EN 1992-1-1:2008 with Polish NA (NDP sources listed on the NDP sheet) |
| National Annex | Selectable: UK NA to BS EN 1992-1-1 or Polish NA to PN-EN 1992-1-1                                        |
| Issued         | 29 October 2026                                                                                           |

## What it does

Effective length of a column in a regular frame from the relative flexibility of the restraints at its two ends (5.15 braced, 5.16 unbraced), its slenderness and the slenderness limit above which second-order effects must be included.

## How to use

1. Open the Calculation sheet and select the National Annex.
2. Fill in the shaded input cells. Everything else is calculated.
3. Read the Results block; every step below it quotes its clause. Print or save as PDF for your calculation package.

## Scope and limitations

Rectangular column, bending about the axis with the depth  $h$  entered, clear height  $l$  between the restraints. At each end: beams (one or two, rectangular gross sections), a fixed foundation ( $k = 0.1$ , the least value of 5.8.3.2(3)) or a pin ( $k = \infty$ ).  $k = (EI / l)_{\text{column}} / \sum \kappa (EI / L)_{\text{beam}}$ , with the column above or below added to the column term when it contributes to the rotation (5.8.3.2(4)),  $\kappa$  the rotational stiffness factor of the beams entered: 4 far end fixed, 3 pinned for uncracked elastic beams; the stiffness of the restraining beams must include cracking unless they are shown to be uncracked at ULS (5.8.3.2(5)), for which  $\kappa = 2$  is a common allowance (TCC guidance).  $E$  the same throughout;  $k$  not less than 0.1. Braced (5.15):  $l_0 = 0.5 l \sqrt{((1 + k_1 / (0.45 + k_1))(1 + k_2 / (0.45 + k_2)))}$ ; unbraced (5.16):  $l_0 = l \max(\sqrt{(1 + 10 k_1 k_2 / (k_1 + k_2)); (1 + k_1 / (1 + k_1))(1 + k_2 / (1 + k_2))})$ . Slenderness  $\lambda = l_0 / i$ ,  $i = h / \sqrt{12}$  (5.14); limit  $\lambda_{\text{lim}} = 20 A B C / \sqrt{n}$  (5.13N) with  $A$  and  $B$  entered (0.7 and 1.1 when not known) and  $C = 1.7 - r_m$ ,  $r_m = M_{01} / M_{02}$  with  $|M_{02}| \geq |M_{01}|$ , positive when both end moments give tension on the same side, negative otherwise.  $r_m = 1$  ( $C = 0.7$ ) is taken for unbraced columns and for braced columns whose first-order moments arise mainly from imperfections or transverse load (5.8.3.1(1));  $n = N_{Ed} / (A_c f_{cd})$ . The second-order design itself is RC-008. Unbraced columns pinned at both ends are unstable and FAIL. The second-generation EN 1992-1-1:2023 is not yet implemented.

## Further reading and independent cross-check

- The Concrete Centre, How to design concrete structures using Eurocode 2: Columns (effective length, slenderness).
- The Concrete Centre, Concise Eurocode 2, 5.6 (slenderness).

NA Engineering is not affiliated with The Concrete Centre or CIRIA; their publications are referenced for information only.

## About NA Engineering

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|          |                                                                                             |
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## Disclaimer

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## Revision history

|      |                           |
|------|---------------------------|
| v1.0 | 29 Oct 2026 · First issue |
|------|---------------------------|

Project  
Element  
Date

Job no.  
Made by  
Checked

**Inputs · column and frame**
*Shaded cells only*

|            | National Annex                                               |           | UK NA (BS EN) |                           |
|------------|--------------------------------------------------------------|-----------|---------------|---------------------------|
| Table 3.1  | Concrete strength class                                      |           | <b>C32/40</b> |                           |
| 5.8.3.2    | Frame                                                        |           | <b>Braced</b> |                           |
|            | Clear height between restraints                              | $l$       | <b>3500</b>   | mm                        |
|            | Column: width $b$                                            | $b$       | <b>400</b>    | mm                        |
|            | Column: depth $h$ (in the direction of buckling)             | $h$       | <b>400</b>    | mm                        |
|            | Beam stiffness factor $\kappa$ in $\kappa EI / L$            | $\kappa$  | <b>2.0</b>    | 4 fixed, 3 pinned far end |
| 5.8.3.2(3) | Top end                                                      |           | <b>Beams</b>  |                           |
|            | Top: number of beams (1 – 2)                                 | $n$       | <b>2</b>      |                           |
|            | Top beam 1: $b \times h \times \text{span}$                  | $b$       | <b>300</b>    | mm                        |
|            |                                                              | $h$       | <b>600</b>    | mm                        |
|            |                                                              | $L$       | <b>6000</b>   | mm                        |
|            | Top beam 2: $b \times h \times \text{span}$                  | $b$       | <b>300</b>    | mm                        |
|            |                                                              | $h$       | <b>600</b>    | mm                        |
|            |                                                              | $L$       | <b>6000</b>   | mm                        |
| 5.8.3.2(4) | Top: column beyond the node, same section (0 = none or not c | $l_{adj}$ | <b>3500</b>   | mm                        |
| 5.8.3.2(3) | Bottom end                                                   |           | <b>Beams</b>  |                           |
|            | Bottom: number of beams (1 – 2)                              | $n$       | <b>2</b>      |                           |
|            | Bottom beam 1: $b \times h \times \text{span}$               | $b$       | <b>300</b>    | mm                        |
|            |                                                              | $h$       | <b>600</b>    | mm                        |
|            |                                                              | $L$       | <b>6000</b>   | mm                        |
|            | Bottom beam 2: $b \times h \times \text{span}$               | $b$       | <b>300</b>    | mm                        |
|            |                                                              | $h$       | <b>600</b>    | mm                        |
|            |                                                              | $L$       | <b>6000</b>   | mm                        |
| 5.8.3.2(4) | Bottom: column beyond the node, same section (0 = none or n  | $l_{adj}$ | <b>0</b>      | mm                        |

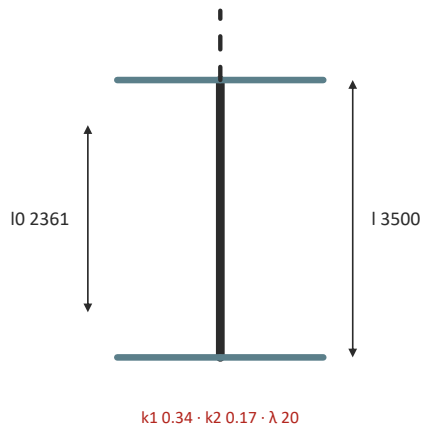
**Inputs · for the slenderness limit**
*Ultimate limit state*

|            |                                                                                |          |                         |           |
|------------|--------------------------------------------------------------------------------|----------|-------------------------|-----------|
|            | Axial force                                                                    | $N_{Ed}$ | <b>2000</b>             | kN        |
| 5.8.3.1(1) | Factor $A = 1 / (1 + 0.2 \phi_{ef})$                                           | $A$      | <b>0.70</b>             |           |
| 5.8.3.1(1) | Factor $B = \sqrt{1 + 2 \omega}$                                               | $B$      | <b>1.10</b>             |           |
| 5.8.3.1(1) | Braced: first-order moments from (unbraced: either, not used)                  |          | <b>End moments only</b> |           |
| 5.8.3.1(1) | End moments: $r_m = M_{01} / M_{02}$ , $ M_{02}  \geq  M_{01} $ (+ same side i | $r_m$    | <b>1.00</b>             |           |
|            | Inputs valid and consistent                                                    |          |                         | <b>OK</b> |

## Results

|                                                 |           |                    |                    |
|-------------------------------------------------|-----------|--------------------|--------------------|
| Effective length                                | $l_o$     | <b>2361</b>        | mm                 |
| Effective length factor                         | $l_{o/l}$ | <b>0.675</b>       |                    |
| Slenderness $\lambda / \lambda_{lim}$ (5.8.3.1) |           | <b>1.57</b>        | Slender: 2nd order |
| Slenderness $\lambda$ and its limit             | $\lambda$ | <b>20.4 / 13.0</b> |                    |

Your column, elevation · clear height  $l$ , the beams framing in at each end (schematic, drawn longer for the longer span), the column beyond a node when counted (dashed),



## Calculation · relative flexibilities

|            |                                                             |                       |           |                 |
|------------|-------------------------------------------------------------|-----------------------|-----------|-----------------|
|            | Column $l / l$ (E cancels)                                  | $l_{c/l}$             | 6.095E+05 | mm <sup>3</sup> |
| 5.8.3.2(3) | Beams at the top $\sum \kappa l / L$                        | $\sum \kappa l_{b/l}$ | 3.600E+06 | mm <sup>3</sup> |
| 5.8.3.2(4) | Column term at the top $l/l + l/l_{adj}$                    | $\sum l_{c/l}$        | 1.219E+06 | mm <sup>3</sup> |
| 5.8.3.2(3) | k at the top ( $\geq 0.1$ ; fixed 0.1, pinned $\infty$ )    | $k_1$                 | 0.339     |                 |
| 5.8.3.2(3) | Beams at the bottom $\sum \kappa l / L$                     | $\sum \kappa l_{b/l}$ | 3.600E+06 | mm <sup>3</sup> |
| 5.8.3.2(4) | Column term at the bottom $l/l + l/l_{adj}$                 | $\sum l_{c/l}$        | 6.095E+05 | mm <sup>3</sup> |
| 5.8.3.2(3) | k at the bottom ( $\geq 0.1$ ; fixed 0.1, pinned $\infty$ ) | $k_2$                 | 0.169     |                 |

## Calculation · effective length and slenderness

|            |                                                                                                |                 |             |             |
|------------|------------------------------------------------------------------------------------------------|-----------------|-------------|-------------|
| (5.15)     | Braced $0.5 l \sqrt{(1 + k_1/(0.45 + k_1))(1 + k_2/(0.45 + k_2))}$                             | $l_{o,br}$      | 2361        | mm          |
| (5.16)     | Unbraced $l \max(\sqrt{(1 + 10 k_1 k_2/(k_1 + k_2)); (1 + k_1/(1 + k_1))(1 + k_2/(1 + k_2))})$ | $l_{o,unbr}$    | 5107        | mm          |
| 5.8.3.2    | Used                                                                                           | $l_o$           | <b>2361</b> | mm          |
| (5.14)     | Slenderness $l_o / i$ , $i = h / \sqrt{12}$                                                    | $\lambda$       | 20.4        |             |
| 2.4.2.4(1) | Partial factor, concrete                                                                       | $\gamma_c$      | 1.50        | NDP sheet   |
| 3.1.6(1)   | Coefficient on compressive strength (flexure)                                                  | $\alpha_{cc}$   | 0.85        | NDP sheet   |
| Table 3.1  | Characteristic cylinder strength                                                               | $f_{ck}$        | 32          | MPa         |
| Table 3.1  | Mean tensile strength                                                                          | $f_{ctm}$       | 3.02        | MPa         |
| (5.13N)    | Relative axial force $NEd / (A_c f_{cd})$                                                      | $n$             | 0.689       |             |
| 5.8.3.1(1) | $C = 1.7 - r_m$ (unbraced, imperfections or transverse load: $r_m = :$                         | $C$             | 0.70        |             |
| (5.13N)    | Limit $20 A B C / \sqrt{n}$                                                                    | $\lambda_{lim}$ | 13.0        |             |
| 5.8.3.1(1) | $\lambda \leq \lambda_{lim}$ : second-order effects may be ignored                             |                 | 20.4        | <b>FAIL</b> |

For a column restrained differently about its two axes, run the sheet once for each axis with  $h$  the depth in that direction. Where a column is pinned at one end  $k = \infty$  is represented by  $10^9$ .

Prepared with NA Engineering calculation tools · [naengineering.uk](http://naengineering.uk) · [adrian@naengineering.uk](mailto:adrian@naengineering.uk). Free for use by competent engineers; see the About sheet for scope and disclaimer.

## Nationally Determined Parameters

Values used by the Calculation sheet for the selected National Annex. Sources: UK NA to BS EN 1992-1-1:2004, Table NA.1; PN-EN 1992-1-1:2008, Załącznik krajowy NA. Edit only if your project specifies different values.

| Parameter                                               | Clause             | UK NA        | PL NA        | Notes                                                                                                     |
|---------------------------------------------------------|--------------------|--------------|--------------|-----------------------------------------------------------------------------------------------------------|
| Partial factor, concrete $\gamma_c$                     | 2.4.2.4(1)         | <b>1.5</b>   | <b>1.4</b>   | Persistent & transient. UK NA: recommended; PL: NA.2, Table NA.2                                          |
| Partial factor, reinforcement $\gamma_s$                | 2.4.2.4(1)         | <b>1.15</b>  | <b>1.15</b>  | UK NA: recommended; PL: NA.2, Table NA.2                                                                  |
| $\alpha_{cc}$ (compression in flexure / axial)          | 3.1.6(1)           | <b>0.85</b>  | <b>1</b>     | UK NA: 0.85; PL: recommended (NA.9)                                                                       |
| $\alpha_{cc,pl}$ (plain concrete, compression)          | 12.3.1(1)          | <b>0.6</b>   | <b>0.8</b>   | UK NA Table NA.1: 0.6; PL: recommended (NA.9)                                                             |
| $\alpha_{cc}$ (shear and punching)                      | 3.1.6(1)           | <b>1</b>     | <b>1</b>     | UK NA: 1.0 for other phenomena; PL: recommended (NA.9)                                                    |
| $\alpha_{ct}$ (design tensile strength)                 | 3.1.6(2)           | <b>1</b>     | <b>1</b>     | Recommended value in both annexes                                                                         |
| CRd,c numerator (CRd,c = value / $\gamma_c$ )           | 6.2.2(1), 6.4.4(1) | <b>0.18</b>  | <b>0.18</b>  | Recommended value in both annexes                                                                         |
| k1 (axial stress term, punching)                        | 6.4.4(1)           | <b>0.1</b>   | <b>0.1</b>   | Recommended value in both annexes                                                                         |
| vRd,max factor (vRd,max = factor · v · fcd)             | 6.4.5(3)           | <b>0.5</b>   | <b>0.4</b>   | UK NA: 0.5 v fcd; PL: recommended value (NA.9), 0.4 v fcd since EN 1992-1-1 AC:2010 (PN-EN 1992-1-1:2008) |
| kmax (vEd ≤ kmax · vRd,c at u1)                         | 6.4.5              | <b>2</b>     | <b>1.5</b>   | UK NA 6.4.5(3): 2 vRd,c. PL: no limit in PN-EN 1992-1-1:2008; 1.5 (A1:2014 recommendation) applied conse  |
| $\phi_{large}$ (large bar threshold, mm)                | 8.8(1)             | <b>40</b>    | <b>32</b>    | UK NA: 40 mm; PL: 32 mm recommended (NA.9)                                                                |
| cot $\theta$ upper limit (variable strut)               | 6.2.3(2)           | <b>2.5</b>   | <b>2</b>     | UK NA: 2.5 (1.25 with axial tension); PL: NA.4, $1 \leq \cot \theta \leq 2.0$                             |
| k1 (x/d limit, $\delta \geq k1 + k2 x_u/d$ )            | 5.5(4)             | <b>0.4</b>   | <b>0.44</b>  | UK NA for $f_{yk} \leq 500$ MPa; PL: recommended (NA.9)                                                   |
| k2 (x/d limit, $\epsilon_{cu2} = 0.0035$ )              | 5.5(4)             | <b>1</b>     | <b>1.25</b>  | UK NA: $0.6 + 0.0014/\epsilon_{cu2}$ ; PL: $1.25(0.6 + 0.0014/\epsilon_{cu2})$                            |
| Upper limit on the (310/ $\sigma_s$ ) factor (0 = none) | 7.4.2(2)           | <b>1.5</b>   | <b>0</b>     | UK NA Table NA.5 Note 5: (310/ $\sigma_s$ ) or (500/ $f_{yk}$ )( $A_s,prov/A_s,req$ ) ≤ 1.5; PL: none     |
| L/d not to exceed 40 K (1 = applies)                    | 7.4.2(2)           | <b>1</b>     | <b>0</b>     | UK NA Table NA.5 Note 6; not in EN text                                                                   |
| $\phi_{min}$ (longitudinal bars in columns, mm)         | 9.5.2(1)           | <b>12</b>    | <b>6</b>     | UK NA: 12 mm; PL: NA.6, 6 mm                                                                              |
| k3 (crack spacing)                                      | 7.3.4(3)           | <b>3.4</b>   | <b>3.4</b>   | Recommended value in both annexes                                                                         |
| k4 (crack spacing)                                      | 7.3.4(3)           | <b>0.425</b> | <b>0.425</b> | Recommended value in both annexes                                                                         |